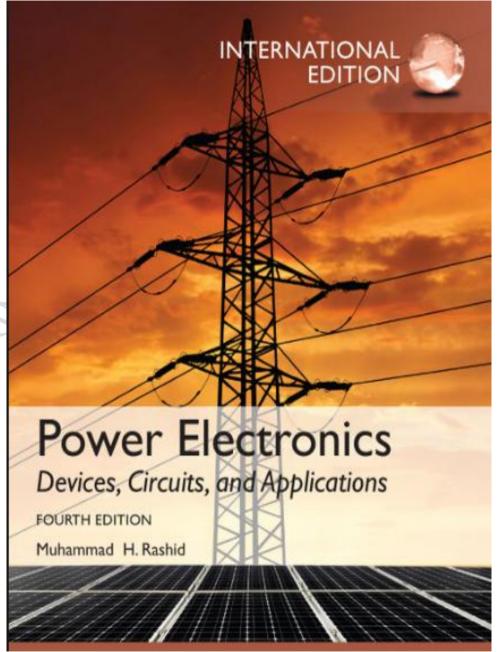
University of Technology Laser and Optoelectronic Engineering Department Power Electronics/2018-2019) For the third years (Laser Engineering)

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Ref: Power Electronics 4th edition/ Muhammed H. Rashid

## Lecture No.7

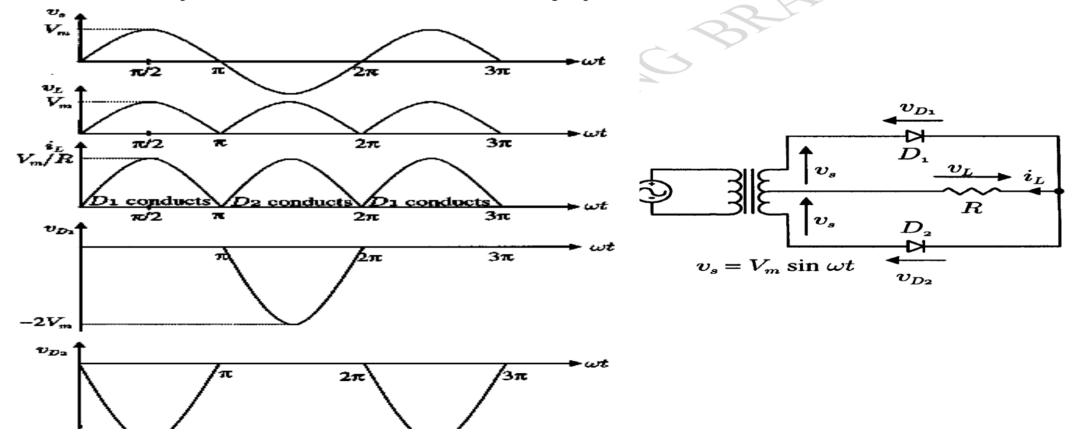
## **Single-Phase Full-Wave Rectifiers**

There are two types of single-phase full-wave rectifier, namely, full-wave rectifiers with center-tapped transformer and bridge rectifiers.

## I. full-wave rectifier with a center-tapped transformer:

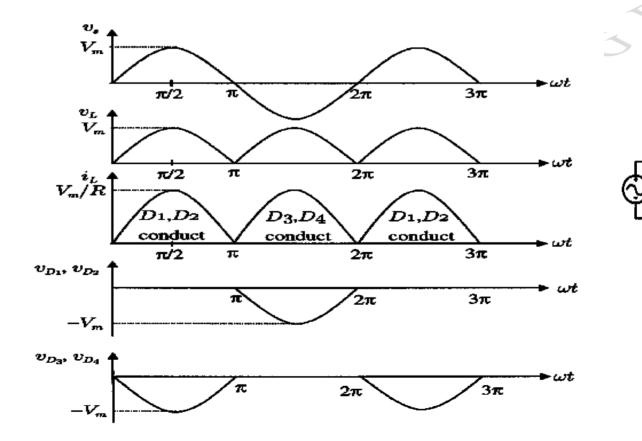
It is clear that each diode, together with the associated half of the transformer, acts as a half-wave rectifier. The outputs of the two half- wave rectifiers are combining to produce full-wave rectification in the load.

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- $\rightarrow$ It is clear that the peak inverse voltage (PIV) of the diodes is equal to  $2V_m$  during their blocking state. Hence, the Peak Repetitive Reverse Voltage (V<sub>RRM</sub>) rating of the diodes must be chose to be higher than  $2V_m$  to avoid reverse breakdown.
- $\rightarrow$ During its conducting state, each diode has a forward current that is equal to the load current and, therefore, the Peak Repetitive Forward Current (I<sub>FRM</sub>) rating of these diodes must be chosen to be higher than the peak load current V<sub>m</sub>=R in practice.

**Bridge rectifier**: It can provide full-wave rectification without using a center-tapped transformer. During the positive half cycle of the transformer secondary voltage, the current flows to the load through diodes  $D_1$  and  $D_2$ . During the negative half cycle,  $D_3$  and  $D_4$  conduct.



 $\imath_L$ 

 $v_L$ 

 $D_1 \ddagger D_3 \ddagger$ 

*D*4本 *D*2本

U.

 $v_s = V_m \sin \omega t$ 

- $\rightarrow$ As with the full-wave rectifier with center-tapped transformer, the Peak Repetitive Forward Current (I<sub>FRM</sub>) rating of the employed diodes must be chosen to be higher than the peak load current V<sub>m</sub>= I<sub>m</sub> ×R
- $\rightarrow$  However, the peak inverse voltage (PIV) of the diodes is reduced from  $2V_m$  to  $V_m$  during their blocking state.

 $V_{dc} = \frac{1}{\pi} \int_0^{\pi} V_m \sin \omega t \, d(\omega t) = V_m |\sin \omega t|$  for both the positive and negative half-cycles. Hence;

Therefore;

Full-wave 
$$V_{\rm dc} = \frac{2V_m}{\pi} = 0.636 V_m$$

The root-mean-square (rms) value of load voltage  $v_L$  is  $V_L$ , which is defined as:

$$V_L = \left[\frac{1}{T}\int_0^T v_L^2(t)dt\right]^{1/2}$$

Hence, the equation can be rewritten as

$$V_L = \sqrt{\frac{1}{\pi}} \int_0^{\pi} (V_m \sin \omega t)^2 d(\omega t)$$

OR

Full-wave 
$$V_L = \frac{V_m}{\sqrt{2}} = 0.707 V_m$$

Therefore; the average and the rms value load current is:

$$I_{\rm dc} = \frac{0.636 \ V_m}{R}$$
$$I_{\rm c} = \frac{0.707 \ V_m}{R}$$

$$I_L = \frac{0.707}{R}$$

The rectification ratio is:

$$\frac{P_{\rm dc}}{P_L} = \frac{V_{\rm dc}I_{\rm dc}}{V_L I_L}$$

$$=\frac{(0.636 V_m)^2}{(0.707 V_m)^2}=81\%$$

The FF can be found by:

$$FF = \frac{V_L}{V_{dc}} \quad or \quad \frac{I_L}{I_{dc}}$$

$$\mathbf{FF} = \frac{0.707 \ V_m}{0.636 \ V_m} = 1.11$$

The ripple factor (RF), which is a measure of the ripple content, is defined as:

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$$\mathbf{RF} = \frac{V_{ac}}{V_{dc}}$$
$$V_{ac} = \sqrt{V_L^2 - V_{dc}^2}$$
$$\mathbf{RF} = \sqrt{\left(\frac{V_L}{V_{dc}}\right)^2 - 1} = \sqrt{\mathbf{FF}^2 - 1}$$

$$RF = \sqrt{1.11^2 - 1} = 0.482$$